

# SO<sub>2</sub> resistant antimony promoted V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst for NH<sub>3</sub>-SCR of NO<sub>x</sub> at low temperatures

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## Abstract

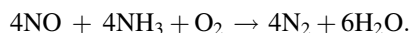
To get the low temperature sulfur resistant V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalysts quantum chemical calculation study was carried out. After selecting suitable promoters (Se, Sb, Cu, S, B, Bi, Pb and P), respective metal promoted V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalysts were prepared by impregnation method and characterized by X-ray diffraction (XRD) and Brunner Emmett Teller surface area (BET-SA). Se, Sb, Cu, S promoted V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalysts showed high catalytic activity for NH<sub>3</sub> selective catalytic reduction (NH<sub>3</sub>-SCR) of NO<sub>x</sub> carried at temperatures between 150 and 400 °C. The conversion efficiency followed in the order of Se > Sb > S > V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> > Cu but Se was excluded because of its high vapor pressure. An optimal 2 wt% ‘Sb’ loading was found over V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> for maximum NO<sub>x</sub> conversion, which also showed high resistance to SO<sub>2</sub> in presence of water when compared to other metal promoters. In situ electrical conductivity measurement was carried out for Sb(2%)/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> and compared with commercial W(10%)/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst. High electrical conductivity difference ( $\Delta G$ ) for Sb(2%)/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst with temperature was observed. SO<sub>2</sub> deactivation experiments were carried out for Sb(2%)/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> and W(10%)/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> at a temperature of 230 °C for 90 h, resulted Sb(2%)/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> was efficient catalyst. BET-SA, X-ray photoelectron spectroscopy (XPS) and carbon, hydrogen, nitrogen and sulfur (CHNS) elemental analysis of spent catalysts well proved the presence of high ammonium sulfate salts over W(10%)/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> than Sb(2%)/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst. © 2007 Elsevier B.V. All rights reserved.

**Keywords:** NO<sub>x</sub> conversion at low temperature; Sb(2%)/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub>; Electrical conductivity; Resistance to SO<sub>2</sub>

## 1. Introduction

Nitrogen oxides (NO<sub>x</sub>) emitted from automobiles and stationary sources such as oil and coal-fired power plants, waste incinerators, industrial ovens and chemical processes. Nearly all NO<sub>x</sub> (95%) derives from transportation (49%) and power plants (46%) [1]. They contribute to photochemical smog, acid rain, ozone depletion and greenhouse effects. The direct health hazards related to NO<sub>x</sub> are bronchitis, pneumonia, viral infections and hay fever. Selective catalytic reduction (SCR) of NO<sub>x</sub> to N<sub>2</sub> using ammonia as a reductant is now considered to be the most effective and common technique to remove the NO<sub>x</sub> in the exhaust gas from stationary sources

[2,3]. The general reaction occurring is



The well known industrial catalyst for this process is based on V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> (anatase) promoted with WO<sub>3</sub>. The required operating temperature for the above industrial catalyst is typically 300–400 °C. This makes it necessary to locate the SCR unit upstream of the desulfurizer and/or particulate control device in order to avoid reheating the flue gas. Despite the low sensitivity of this catalyst to SO<sub>2</sub> poisoning, deactivation does occur. The life of the catalyst is shortened because of high concentrations of SO<sub>2</sub> and ash in the flue gas. This can be avoided by locating the SCR unit at the very end of the flue gas pollution abatement units where the flue gas is relatively clean as it passes through the scrubber and the electrostatic precipitator or bag-house. Therefore, in certain circumstance where flue gas temperature is low, it is necessary to develop a catalyst which shows high activity at a lower reaction

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temperature. A low temperature SCR process is believed to have low energy consumption and to be economical for retrofitting into the existing units for flue gas cleaning. The key to development of the low temperature SCR process is SCR catalysts of high resistance to  $\text{SO}_2$  poisoning because the formation of the ammonium bisulfate salts on the catalyst surface is serious at low temperatures [4].

Several types of low temperature active catalysts have been developed [5–8]. However, they have poor durability under sulfur and water environments. Some supported transition metal oxide catalysts have been investigated for the low temperature SCR reactions, which are capable of operating at the low temperature range between 80 and 250 °C. Amorphous chromia [9], carbon-supported vanadium [10,11], manganese [12] and copper [5,6] oxides, alumina supported manganese oxide [13],  $\text{TiO}_2$  supported chromia [14], vanadium and copper-nickel oxides supported on titania and alumina monoliths [15], show high activity for NO reduction with  $\text{NH}_3$  at low temperatures. Peña et al. [16] reported that the catalytic performance of titania supported V, Cr, Mn, Fe, Co, Ni and Cu catalysts followed the order of  $\text{Mn} > \text{Cu} > \text{Cr} > \text{Co} > \text{Fe} > \text{V} > \text{Ni}$  for low temperature (80–250 °C) SCR of NO with  $\text{NH}_3$ . These catalysts have the drawback of  $\text{SO}_2$  poisoning in the presence of water and it was reported that chemical transformation of MnO to  $\text{MnSO}_4$  was the main reason for deactivation of SCR over  $\text{MnO}_x/\text{Al}_2\text{O}_3$  [17].

Generally, when titanium dioxide ( $\text{TiO}_2$ ) supporters and vanadium (V) used as active catalytic materials, the additional amount of vanadium is added to increase the catalytic activity at 300 °C or lower. However, when the amount of vanadium increased, the oxidation of sulfur dioxide ( $\text{SO}_2$ ) to sulfur trioxide ( $\text{SO}_3$ ) is induced, which further reacts with slipped ammonia. As a result ammonium bisulfate ( $\text{NH}_4\text{HSO}_4$ ), a solid salt formed over the catalyst surface and interfere the SCR reaction. Hence the amount of unreacted ammonia increases, formation of sulfur trioxides ( $\text{SO}_3$ ) is promoted, thereby accelerating the sulfur poisoning, which eventually shortens the life of the catalysts. Therefore, catalysts that can improve catalytic activity at low temperatures without promoting the oxidation of sulfur dioxides need to be developed.

In the case of  $\text{V}_2\text{O}_5/\text{Al}_2\text{O}_3$  [18], formation of aluminum sulfate during SCR reaction in the presence of  $\text{SO}_2$  reduces surface area of the catalyst sorbents, which results in severe deactivation of SCR activity.  $\text{NH}_4\text{HSO}_4$  was also found to accumulate on the surface of  $\text{V}_2\text{O}_5/\text{TiO}_2$  [19,20],  $\text{V}_2\text{O}_5/\text{AC}$  [21,22], and CuHM [23] at temperatures below 280 °C which inhibits SCR activity due to pore plugging. Conventionally, in order to enhance low temperature activity and sulfur poisoning resistance, tungsten has been added to  $\text{V}_2\text{O}_5/\text{TiO}_2$  catalysts as a promoter [19,24–26]. When tungsten (W) used as promoter it could be important to increase the percentage of tungsten approximately 5–10 wt% to get the low temperature sulfur poisoning resistance. However, the amount of tungsten increases the price of the catalyst. Our aim is to find a promoter which can replace tungsten as well as to improve the sulfur poisoning at low temperatures.

In the present study, quantum chemical calculation was carried out to choose promoters which can replace tungsten. In situ electrical conductivity studies were carried out for the promoted  $\text{V}_2\text{O}_5/\text{TiO}_2$  catalysts before and after the exposure of mixture gas and difference in the electrical conductivity ( $\Delta G$ ) values were correlated with the  $\text{NO}_x$  conversion efficiencies.  $\text{SO}_2$  deactivation experiments with time on stream were also carried for the catalysts chosen and compared with commercial  $\text{W}(10\%)/\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst. X-ray photoelectron spectroscopy (XPS), Brunner Emmett Teller surface area (BET-SA) and carbon, hydrogen, nitrogen and sulfur (CHNS) elemental analysis were carried out to analyze the presence of ammonium bisulfate salt which is main cause for  $\text{SO}_2$  poisoning effect.

## 2. Experimental

### 2.1. Quantum chemical studies

Adsorption of ammonium bisulfate on the  $\text{V}_2\text{O}_5/\text{TiO}_2$  promoted by metal (M) was modeled as described in Fig. 1. Quantum chemical calculation was carried out using indigenous Spanish initiative for electronic simulations with thousands of atoms (SIESTA) software to estimate bonding strengths between ammonium bisulfate and transition metals. From this quantum chemical calculations the best metals which have weak bond strength were screened from the periodic table and selected for the  $\text{NH}_3$ -SCR to reduce the low temperature sulfur dioxide deactivation caused by the formation of ammonium bisulfate salts over metal promoted  $\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst.

### 2.2. Catalyst preparation

The commercial  $\text{TiO}_2$  (DT-51 Millennium Chemicals) powder was used as support for the preparation of all catalysts. The  $\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst was prepared by wet impregnation of vanadia on titania by using ammoniummetavanadate ( $\text{NH}_4\text{VO}_3$ ) (99% pure Junsei chemicals) precursor. The required amount of ammoniummetavanadate was added to the oxalic acid solution and heated to dissolve ammoniummetavanadate. To this solution the calculated amount of titania (DT-51) powder was added and stirred for an hour followed by evaporation, drying and calcination at 400 °C for 4 h in air. Following the same procedure a series of  $\text{MO}_x\text{-V}_2\text{O}_5/\text{TiO}_2$  catalysts were prepared by

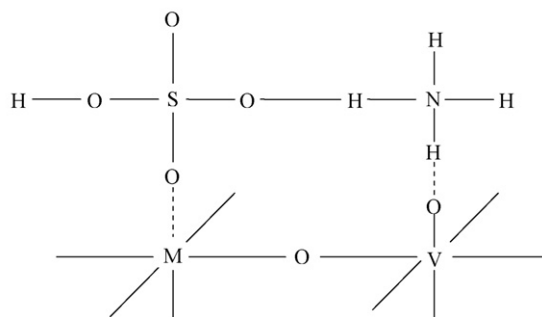


Fig. 1. Modeling for the adsorption of ammonium bisulfate over  $\text{V}_2\text{O}_5\text{-MO}_x/\text{TiO}_2$ .

using different metal (Se, Sb, Cu, S, B, Bi, Pb and P) precursor salts (99% pure Aldrich chemicals). Commercial W(10%)/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst supplied by Kerr McGee was used as it is.

### 2.3. Characterization

All the prepared catalysts were analyzed by powder X-ray diffractometer (XRD) (Bruker) and spectra were recorded using a Ni filtered Cu K $\alpha$  radiation, operated at 40 kV and 20 mA. The fine powders were scanned in the  $2\theta$  range from 20 to 80. BET-SA of the prepared catalysts were measured from N<sub>2</sub> adsorption isotherms at  $-196^\circ\text{C}$  using a micromeritics (Autochem-II 2920) analyzer. X-ray photo electronic spectrographs (XPS) (recorded by using PHI 5800 ESCA system), BET-SA (Autochem-II 2920) and elemental analysis (by using Perkin-Elmer 2400 series II CHNS analyzer) were analyzed for the spent catalysts as post-characterization study.

### 2.4. Electrical conductivity measurements

The electrical conductivity ( $\sigma$ ) measurements were carried under vacuum conditions using inbuilt setup (Fig. 2) consisting of a cell with platinum electrodes, thermocouple, heating coil and electrometer (Keithley 6517A) using following procedure: (a) 400 mg of the catalyst was loaded in between the circular platinum electrodes in the cell (b) evacuation of the cell and preheating of the catalyst was carried to remove the water and physically adsorbed gases at  $150^\circ\text{C}$  for 2 h (c) after cooling to room temperature,  $400\text{ cm}^3$  of pure oxygen gas ( $5.5 \times 10^2\text{ Pa}$ ) was introduced and maintained the desired reaction temperature with a ramp of  $5^\circ\text{C min}^{-1}$  (e) evacuation of the cell was done and electrical conductivity ( $\sigma$ ) of the loaded catalyst were measured by introducing pure reactant gases into the cell at the respective reaction temperatures using the formula [27]

$$\sigma = \frac{t}{RS}$$

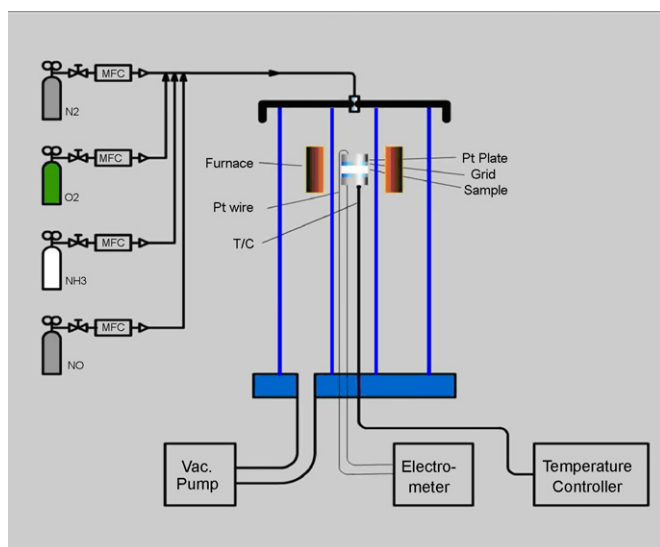


Fig. 2. Diagram of electrical conductivity measurement unit.

where  $\sigma$  is the conductivity,  $t$  the thickness of the loaded catalyst between circular platinum electrodes,  $R$  the resistance and  $S$  is the cross-sectional area of the circular platinum electrodes.

### 2.5. Activity measurements

Catalytic activity measurements were (carried with and without SO<sub>2</sub> in presence of water) performed in a dynamic on-line micro reactor using a feed stream consisting of 800 ppm NO<sub>x</sub>, 800 ppm NH<sub>3</sub>, 3 vol% O<sub>2</sub>, 6 vol% H<sub>2</sub>O, 500 ppm SO<sub>2</sub> and nitrogen balance in the temperature range between 150 and  $400^\circ\text{C}$ , with a total flow rate of  $500\text{ cm}^3\text{ min}^{-1}$  and at a space velocity of  $60,000\text{ h}^{-1}$ . The catalysts particle size of 300–425  $\mu\text{m}$  were used for activity measurements and about 250 mg of the catalyst was inserting into the middle of quartz tube supporting by quartz wool which was positioned middle of the reactor. The effluent from the reactor was analyzed by an online NDIR Fuji NO and SO<sub>2</sub> analyzer. NO conversion was calculated by using the formula given below. The sulfur deactivation studies with time on stream were also carried out and compared with commercial W(10%)/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst at low temperatures.

$$\text{NO conversion} = \frac{\text{NO}_{\text{in}} - \text{NO}_{\text{out}}}{\text{NO}_{\text{in}}} \times 100$$

## 3. Results and discussion

### 3.1. Screening of metals by quantum chemical calculation

Quantum chemical calculation was carried out to estimate bonding strength between ammonium bisulfate and for the different metals in the periodic table. An adsorption model of ammonium bisulfate to V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalysts [28] was schematically shown in Fig. 1. The diagram shows the ammonium bisulfate adsorption on to the V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> surface where TiO<sub>2</sub> surface is covered by V<sub>2</sub>O<sub>5</sub> and a transition metal where Ti is replaced with an arbitrary atom M. In the model, the bonding strength of M $\cdots$ O, which has normally stronger bond than adjacent H $\cdots$ O bond, plays a critical role on the sulfur poisoning. As the bonding strength becomes weaker (M $\cdots$ O), ammonium bisulfate salt can be easily desorbed. From the quantum chemical calculation, suitable metal promoters like Se, Sb, Cu, S, B, Bi, Pb and P were selected on the basis of bond energy (M $\cdots$ O) which may favors the weaker bonding strength (M $\cdots$ O), thus leads to easy desorption of adsorbed ammonium bisulfate salt formed during NH<sub>3</sub>-SCR of NO<sub>x</sub> reaction over the catalyst surface at low temperatures. Among all the selected metal promoters, the order of bonding energy decreased as Pb > B > Bi > Cu > Sb > Se > S > P (Table 1). Taking in to the consideration of order, the best candidate metals 'S' and 'P' showed too low NO<sub>x</sub> reduction, and next candidate 'Se' showed very poor resistance to SO<sub>2</sub> deactivation because of its high vapor pressure at the reaction temperature. Next best candidate 'Sb' showed high activity as well as high resistance to SO<sub>2</sub> deactivation among all. This is further explained in detail coming sections.

Table 1  
The quantum chemical calculation results

Element	Bond energy (eV)
Selenium (Se)	+2.940
Antimony (Sb)	+3.129
Copper (Cu)	+3.158
Sulfur (S)	+2.770
Boron (B)	+3.721
Bismuth (Bi)	+3.509
Lead (Pb)	+3.711
Phosphorous (P)	+2.501

### 3.2. Characterization

The prepared catalysts (Se, Sb, Cu, S, B, Bi, Pb and P doped  $V_2O_5/TiO_2$ ) were characterized by XRD and BET-SA. The XRD spectra of all the catalysts showed the anatase  $TiO_2$  phases at  $2\theta$  of 25.3, 38.0 and 48.0, but the  $V_2O_5$  phases were not observed because of high dispersion and very low percentage ( $V_2O_5(2\%)/TiO_2$ ) of metal content used in preparation of catalysts. Similarly with the addition of promoters to the  $V_2O_5(2\%)/TiO_2$  it is observed that there is no change in the XRD patterns and no specific phases were observed corresponding to the promoters. The composition of the different promoters and  $V_2O_5$  on  $TiO_2$  and BET-SA of the all catalysts are given in Table 2. It could be seen that the highest surface area is obtained for the support  $TiO_2$ , the values changed with addition of the promoters to the  $V_2O_5/TiO_2$  which is expected. XPS and CHNS elemental analysis were done for the spent catalysts after 90 h sulfur deactivation study and the observations were discussed further in Section 3.6.

### 3.3. Influence of promoters on SCR activity in the presence of oxygen

Fig. 3 shows the  $NO_x$  conversion of different metal promoted  $V_2O_5/TiO_2$  catalysts with temperature. The activity was carried in the temperature range from 150 to 400 °C with the reaction mixture containing 800 ppm  $NO_x$ , 800 ppm  $NH_3$ , 3%  $O_2$  at a space velocity of 60,000  $h^{-1}$ . The results show that considerable increase in reaction rate at low temperatures (150–300 °C).

Table 2  
Composition and BET-SA of the catalysts

Catalyst	Composition		BET-SA ( $m^2 g^{-1}$ )
	$V_2O_5$ (%)	$MO_x$ (%)	
$TiO_2$	–	–	94
$V_2O_5/TiO_2$	2	–	91
1% Se/ $V_2O_5/TiO_2$	2	1	90
1% Sb/ $V_2O_5/TiO_2$	2	1	91
2% Sb/ $V_2O_5/TiO_2$	2	2	89
1% Cu/ $V_2O_5/TiO_2$	2	1	87
1% S/ $V_2O_5/TiO_2$	2	1	89
1% B/ $V_2O_5/TiO_2$	2	1	85
1% Bi/ $V_2O_5/TiO_2$	2	1	87
1% Pb/ $V_2O_5/TiO_2$	2	1	87
1% P/ $V_2O_5/TiO_2$	2	1	85

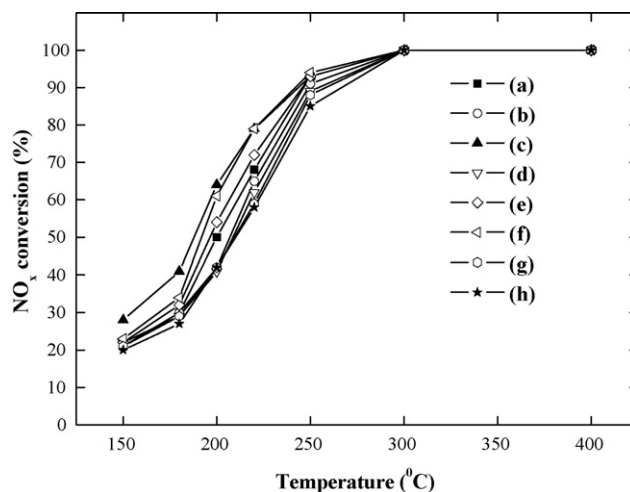


Fig. 3.  $NO_x$  conversion vs. temperature over (a)  $V_2O_5/TiO_2$ , (b) 1% Cu/ $V_2O_5/TiO_2$ , (c) 1% Se/ $V_2O_5/TiO_2$ , (d) 1% Pb/ $V_2O_5/TiO_2$ , (e) 1% S/ $V_2O_5/TiO_2$ , (f) 1% Sb/ $V_2O_5/TiO_2$ , (g) 1% B/ $V_2O_5/TiO_2$  and (h) 1% P/ $V_2O_5/TiO_2$  (conditions: 800 ppm  $NO_x$ , 800 ppm  $NH_3$ , 3 vol%  $O_2$ , S.V.—60,000  $h^{-1}$ ).

$NO_x$  conversion of all catalysts increased with increasing temperature and achieved almost 100%  $NO_x$  conversion at 300 °C. The difference in the conversion was observed at low temperatures below 250 °C. Among all the catalysts, selenium (Se) showed the highest  $NO_x$  conversion at low temperatures and antimony (Sb) followed it. The low temperature  $NO_x$  conversions of Se, Sb, Cu and S promoted  $V_2O_5/TiO_2$  catalysts followed Se > Sb > S >  $V_2O_5/TiO_2$  > Cu order. The  $V_2O_5/TiO_2$  catalyst obtained 50% conversion at a low temperature of 200 °C where as Se/ $V_2O_5/TiO_2$  obtained 64% of conversion and Se/ $V_2O_5/TiO_2$  of 61%.

### 3.4. Influence of promoters on SCR activity in the presence of water and oxygen

Six percent of  $H_2O$  was introduced into the feed to check the influence of water on  $NO_x$  reduction activity. We observed that the NO removal efficiency under dry conditions is higher than wet conditions at a low temperature region on both  $V_2O_5/TiO_2$  and metal promoted  $V_2O_5/TiO_2$  catalysts. This result agrees with the view of most researchers [29–31]. The activity at higher temperatures is not changed above 250 °C and the  $NO_x$  conversion obtained nearly 100%. The activity in the low temperature range of 150–250 °C was decreased to some extent because of competitive adsorption of  $H_2O$  and the reactants,  $NH_3$  and/or NO, but the catalyst is not deactivated. Fig. 4 indicates the water effect on the  $NO_x$  reduction for the  $V_2O_5/TiO_2$  and different metal promoted  $V_2O_5/TiO_2$  catalysts. Among all the catalysts the  $NO_x$  conversion of  $V_2O_5/TiO_2$ , Se, Sb, Cu and S promoted  $V_2O_5/TiO_2$  catalysts followed an order of Se > Sb > S >  $V_2O_5/TiO_2$  > Cu similarly as in dry conditions (Fig. 3) but varied in percent conversion which seems to be slightly less in efficiency in presence of water. Even though selenium (Se) is best promoter for  $NO_x$  conversion but its usage is limited because of its high vapor pressure, hence antimony (Sb) was taken as the best promoter. The  $V_2O_5/TiO_2$



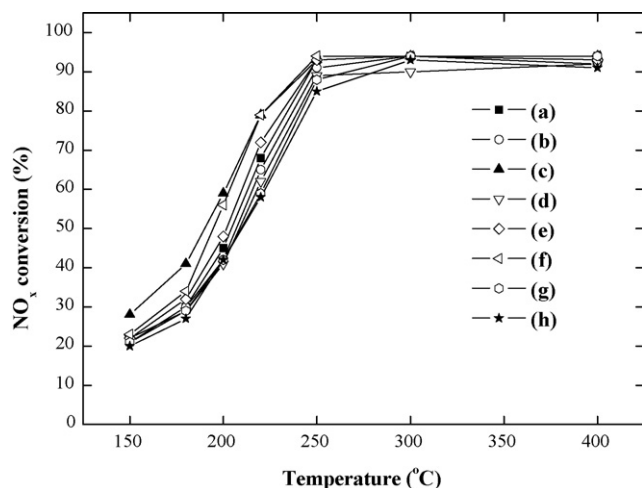


Fig. 4.  $\text{NO}_x$  conversion vs. temperature over (a)  $\text{V}_2\text{O}_5/\text{TiO}_2$ , (b) 1%  $\text{Cu}/\text{V}_2\text{O}_5/\text{TiO}_2$ , (c) 1%  $\text{Se}/\text{V}_2\text{O}_5/\text{TiO}_2$ , (d) 1%  $\text{Pb}/\text{V}_2\text{O}_5/\text{TiO}_2$ , (e) 1%  $\text{S}/\text{V}_2\text{O}_5/\text{TiO}_2$ , (f) 1%  $\text{Sb}/\text{V}_2\text{O}_5/\text{TiO}_2$ , (g) 1%  $\text{B}/\text{V}_2\text{O}_5/\text{TiO}_2$  and (h) 1%  $\text{P}/\text{V}_2\text{O}_5/\text{TiO}_2$  (conditions: 800 ppm  $\text{NO}_x$ , 800 ppm  $\text{NH}_3$ , 3 vol%  $\text{O}_2$ , 6 vol%  $\text{H}_2\text{O}$ ; S.V.—60,000  $\text{h}^{-1}$ ).

catalyst obtained 45% conversion at a low temperature of 200 °C where as  $\text{Se}/\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst obtained 59% of conversion and  $\text{Sb}/\text{V}_2\text{O}_5/\text{TiO}_2$  of 56%. Fig. 5 shows the different percentages of antimony promoted  $\text{V}_2\text{O}_5/\text{TiO}_2$  catalysts in the presence of water. Among 1, 2, 3%  $\text{Sb}/\text{V}_2\text{O}_5/\text{TiO}_2$  catalysts the 2%  $\text{Sb}/\text{V}_2\text{O}_5/\text{TiO}_2$  showed high activity. With the increasing amount of antimony the low temperature activity enhanced up to the 2%. However, activity decreased with further addition of antimony more than 2%. When the amount of antimony is more than 3%, activity was even poorer than that of the  $\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst, which does not contain antimony. It seems that antimony covers the vanadia as well as  $\text{TiO}_2$  when the amount of antimony is higher than 2%. Therefore, it can be observed that optimum amount of antimony is around 2%, which has high dispersion.

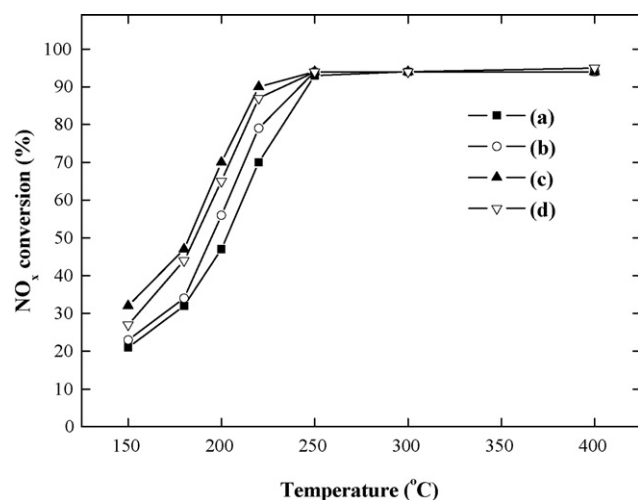


Fig. 5.  $\text{NO}_x$  conversion vs. temperature over (a)  $\text{V}_2\text{O}_5/\text{TiO}_2$ , (b) 1%  $\text{Sb}/\text{V}_2\text{O}_5/\text{TiO}_2$ , (c) 2%  $\text{Sb}/\text{V}_2\text{O}_5/\text{TiO}_2$  and (d) 3%  $\text{Sb}/\text{V}_2\text{O}_5/\text{TiO}_2$  (conditions: same as in Fig. 4).

### 3.5. Electrical conductivity study

It has been reported that  $\text{NO}_x$  conversion is closely related to the behavior of labile oxygen [27,32,33] which will be responsible for increase of electrical conductivities over the catalyst surfaces by the production of anionic vacancies which will be further responsible to react with surrounding anionic pollutants prevailing by introduction of reaction mixture gases during SCR reaction.

Therefore, it is thought that the difference in electrical conductivity ( $\Delta G$ ) over the catalysts surface, before and after introduction of reaction mixture gases could be the measure of an amount of labile oxygen activation. Hence electrical conductivity measurement studies were carried out for both the Sb(2%) and W(10%) promoted catalysts and their  $\text{NO}_x$  conversion efficiencies were compared at temperatures between 150 and 300 °C correlating with the obtained  $\Delta G$  values.

Table 3 shows that the electrical conductivity increases with temperature. This indicates that the samples are in semi-conducting temperature region where conduction takes place mainly through the excitation of electrons at impurity levels. The excitation of electrons is promoted as temperature increases. The electrical conductivity values of Sb(2%)/ $\text{V}_2\text{O}_5/\text{TiO}_2$  and W(10%)/ $\text{V}_2\text{O}_5/\text{TiO}_2$  catalysts at different temperatures were measured. It gives an important evidence of higher  $\Delta G$  value for Sb(2%) promoter catalyst than for W(10%) promoted catalyst at low temperature (230 °C) which also gives well supported reason for the high conversion rates of Sb(2%)/ $\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst than that of commercial W(10%)/ $\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst.

### 3.6. Low temperature $\text{SO}_2$ deactivation studies

In order to determine deactivation characteristics,  $\text{NO}_x$  conversions were measured with the introduction of 500 ppm  $\text{SO}_2$  along with 800 ppm of  $\text{NO}$ , 800 ppm of  $\text{NH}_3$ , 6%  $\text{H}_2\text{O}$  and 3%  $\text{O}_2$ . The low temperature  $\text{SO}_2$  deactivation studies were carried out for the metal promoted  $\text{V}_2\text{O}_5/\text{TiO}_2$  catalysts which showed high  $\text{NO}_x$  conversions. Among the several metal promoted catalysts Se, Sb, Cu and S showed high  $\text{NO}_x$  conversions. The  $\text{SO}_2$  deactivation studies were performed at 240 °C and the Se, Sb, Cu and S promoted catalysts were compared with  $\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst. Fig. 6 explains the effect of  $\text{SO}_2$  on  $\text{NO}_x$  reduction over Se, Sb, Cu, and S promoted  $\text{V}_2\text{O}_5/\text{TiO}_2$  catalysts and  $\text{V}_2\text{O}_5/\text{TiO}_2$ . The  $\text{SO}_2$  deactivation is more serious on the copper (Cu) promoted catalyst than other catalysts as Cu can easily form the  $\text{CuSO}_4$  which enhances the formation and existence of high amounts of ammonium bisulfate salts hence high deactivation occurred. This is in agreement with the order of bonding energy ( $\text{M}\cdots\text{O}$ ) of the metal promoters ( $\text{Cu} > \text{Sb} > \text{Se} > \text{S}$ ) described in Section 3.1. Selenium catalysts also showed deactivation after 4 h because of its high vapor pressure. Best performance was obtained over antimony (Sb) promoted catalyst than the  $\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst. The amount of unreacted ammonia becomes very small and the amount of emitted sulfur dioxide is nearly similar to the amount

Table 3  
 $\Delta G$  and %NO<sub>x</sub> conversions of W/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> and Sb/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalysts with temperature

Catalyst	Temperature (°C)	Electrical conductivity (m <sup>-1</sup> Ω <sup>-1</sup> )		$\Delta G$	%NO <sub>x</sub> conversion
		Before gas supply	After gas supply		
W/V <sub>2</sub> O <sub>5</sub> /TiO <sub>2</sub>	180	$1.6 \times 10^{-11}$	$2.0 \times 10^{-10}$	$1.8 \times 10^{-10}$	45
	200	$1.4 \times 10^{-10}$	$8.0 \times 10^{-10}$	$6.5 \times 10^{-10}$	54
	230	$1.3 \times 10^{-10}$	$9.6 \times 10^{-10}$	$8.3 \times 10^{-10}$	77
	250	$4.2 \times 10^{-10}$	$3.0 \times 10^{-9}$	$2.6 \times 10^{-9}$	100
	300	$1.0 \times 10^{-9}$	$3.8 \times 10^{-8}$	$3.7 \times 10^{-8}$	100
Sb/V <sub>2</sub> O <sub>5</sub> /TiO <sub>2</sub>	180	$7.2 \times 10^{-11}$	$3.0 \times 10^{-10}$	$2.3 \times 10^{-10}$	50
	200	$1.7 \times 10^{-10}$	$9.2 \times 10^{-10}$	$7.5 \times 10^{-10}$	61
	230	$2.4 \times 10^{-9}$	$1.5 \times 10^{-9}$	$1.0 \times 10^{-9}$	89
	250	$6.5 \times 10^{-9}$	$9.4 \times 10^{-8}$	$8.7 \times 10^{-8}$	100
	300	$9.5 \times 10^{-8}$	$9.8 \times 10^{-7}$	$8.8 \times 10^{-7}$	100

introduced, it could be inferred that almost no oxidation of sulfur dioxide occurred within 16 h. This result clearly shows that antimony plays as a promoter enhancing the SO<sub>2</sub> poisoning resistance.

Fig. 7 shows the effect of antimony percentage on the SO<sub>2</sub> deactivation. With the addition of antimony, SO<sub>2</sub> deactivation is reduced and in all cases the antimony promoted catalyst showed best resistance to SO<sub>2</sub> deactivation than the V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst. The 2% Sb/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst is optimized as it showed higher resistance to SO<sub>2</sub> deactivation than 1 and 3% of antimony catalysts up to 18 h. Increasing the percentage of antimony more than 2% caused decreasing the sulfur (SO<sub>2</sub>) resistance. As shown in Fig. 8, deactivation starts early as the reaction temperature decreases to low temperatures. The V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst used to check the effect of SO<sub>2</sub> deactivation at low temperatures. When SO<sub>2</sub> deactivation study is carried at 220 °C the catalyst was poorly resistant to SO<sub>2</sub>, but in the case of 240 and 250 °C the SO<sub>2</sub> resistance increased. At 220 °C the NO<sub>x</sub> conversion is very low and the leftover ammonia can react easily with sulfur dioxide and water to favor the formation of ammonium bisulfate salt which can block the active sites and finally deactivates the catalyst.

Finally, sulfur (SO<sub>2</sub>) deactivation behavior of Sb(2%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> was compared with W(10%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> commercial catalyst and SO<sub>2</sub> deactivation study was carried out at 230 °C for about 90 h and it was shown in Fig. 9. It is observed that the SO<sub>2</sub> resistance was higher for Sb(2%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> than W(10%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst. After 90 h of reaction the spent catalysts were analyzed by BET-SA, XPS and CHNS elemental analysis and the results found were correlated well with the deactivation behaviors of the catalysts.

The measured surface area values (Table 4) of fresh and spent catalysts of W(10%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> and Sb(2%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> also support the reason for decrease of catalytic activity [21] with decreasing the surface area of the catalysts. Surface area of the W(10%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst reduced more than that of Sb(2%) promoted catalyst. This observation explains that the high catalytic activity of Sb(2%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> than W(10%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> at low temperatures is may be due to formation of higher amount of ammonium bisulfate salt over W(10%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> than Sb(2%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub>, causing more difference in reduction of surface area of W(10%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> (Table 4).

The XPS spectra (Fig. 10(A and B)) obtained for the spent Sb(2%) and W(10%) promoted V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalysts are

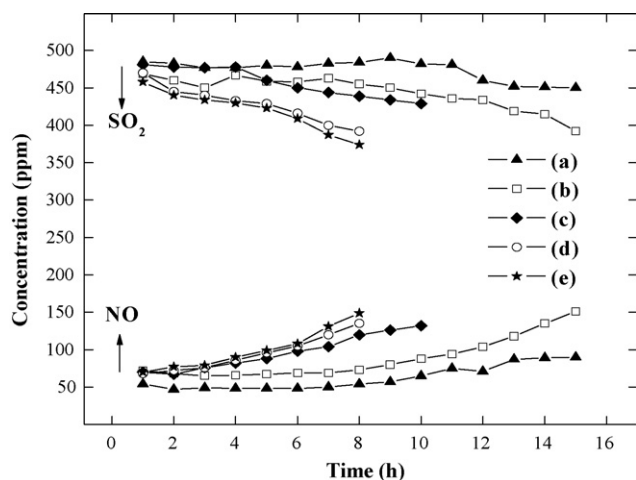


Fig. 6. SO<sub>2</sub> deactivation study at 240 °C over (a) 1% Sb/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub>, (b) V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub>, (c) 1% Se/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub>, (d) 1% S/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> and (e) 1% Cu/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> (conditions: 800 ppm NO<sub>x</sub>, 800 ppm NH<sub>3</sub>, 3 vol% O<sub>2</sub>, 6 vol% H<sub>2</sub>O, 500 ppm SO<sub>2</sub>, S.V.—60,000 h<sup>-1</sup>).

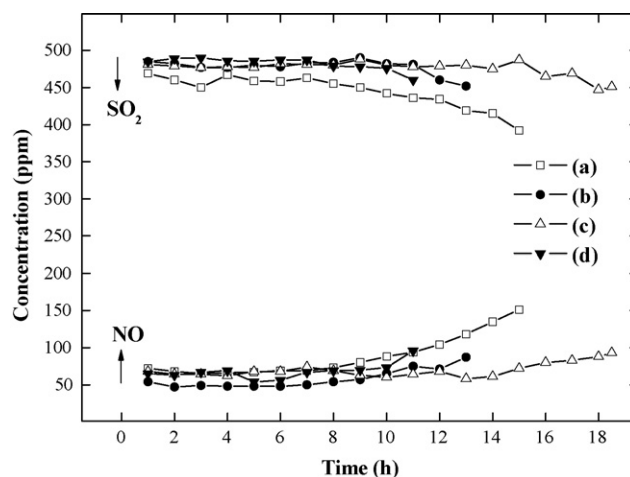


Fig. 7. SO<sub>2</sub> deactivation study at 240 °C over (a) V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub>, (b) 1% Sb/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub>, (c) 2% Sb/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> and (d) 3% Sb/V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> (conditions: same as in Fig. 6).

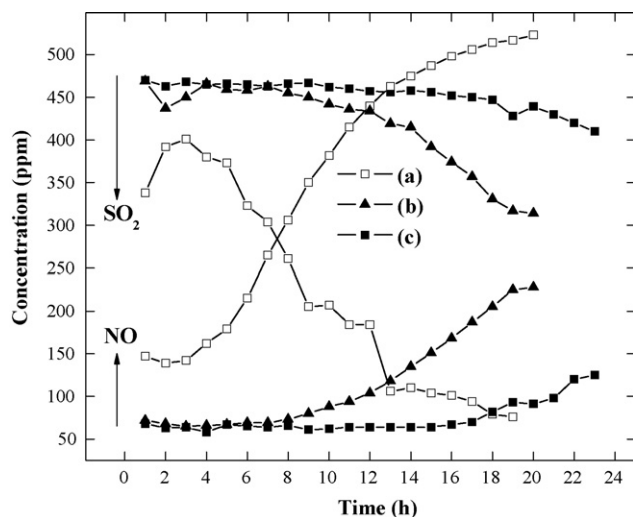


Fig. 8.  $\text{SO}_2$  deactivation study over  $\text{V}_2\text{O}_5/\text{TiO}_2$  catalysts at different temperatures (a)  $220^\circ\text{C}$ , (b)  $240^\circ\text{C}$  and (c)  $250^\circ\text{C}$  (conditions: same as in Fig. 6).

Table 4  
BET-SA of fresh and spent catalysts after 90 h of  $\text{SO}_2$  deactivation

Catalyst	BET-SA ( $\text{m}^2\text{g}^{-1}$ )	
	Fresh	After 90 h deactivation
$\text{Sb}(2\%)/\text{V}_2\text{O}_5/\text{TiO}_2$	89	62
$\text{W}(10\%)/\text{V}_2\text{O}_5/\text{TiO}_2$	85	45

showing the existence of ammonium bisulfate peaks, observed by the presence of S 2p spectra at binding energy of 168.2 eV [34] and N 1s spectra at binding energy of 401.8 eV [35]. The high intensities of the S 2p and N 1s peaks for commercial  $\text{W}(10\%)/\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst observed from the XPS spectra confirming that the existence of high amount of ammonium bisulfates over the catalyst surface than the  $\text{Sb}(2\%)/\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst. It is also confirmed by high atomic weight percentages of nitrogen and sulfur over  $\text{W}(10\%)/\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst surface obtained through XPS analysis (Table 5).

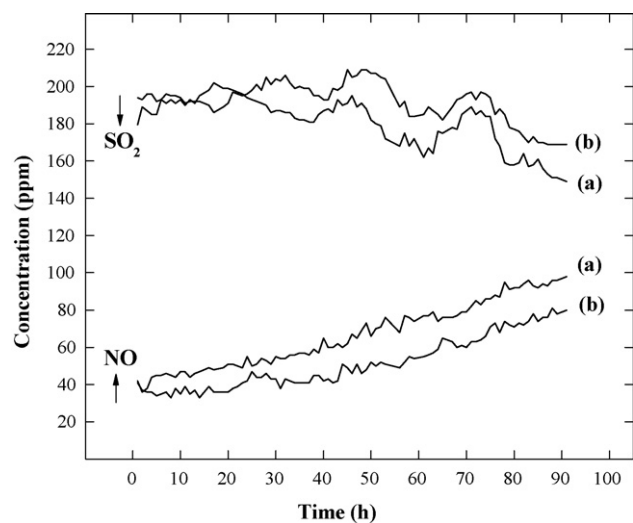


Fig. 9.  $\text{SO}_2$  deactivation study at  $230^\circ\text{C}$  over (a)  $\text{W}(10\%)/\text{V}_2\text{O}_5/\text{TiO}_2$  and (b)  $\text{Sb}(2\%)/\text{V}_2\text{O}_5/\text{TiO}_2$  (conditions: 200 ppm  $\text{NO}_x$ , 200 ppm  $\text{NH}_3$ , 3 vol%  $\text{O}_2$ , 12 vol%  $\text{H}_2\text{O}$ , 200 ppm  $\text{SO}_2$ , S.V.— $60,000\text{ h}^{-1}$ ).

Table 5

Atomic weight percentages of ammonium bisulfate salt formed after 90 h  $\text{SO}_2$  deactivation

Catalyst	S (wt%)		N (wt%)		H (wt%)
	CHNS	XPS	CHNS	XPS	
$\text{W}(10\%)/\text{V}_2\text{O}_5/\text{TiO}_2$	5.07	4.53	4.83	4.42	1.75
$\text{Sb}(2\%)/\text{V}_2\text{O}_5/\text{TiO}_2$	2.97	2.54	2.21	2.04	1.02

The sulfur, nitrogen, hydrogen contents were measured from the CHNS elemental analysis for spent catalysts and the values are given in Table 5. The weight percentages of sulfur, nitrogen, hydrogen were higher for the  $\text{W}(10\%)/\text{V}_2\text{O}_5/\text{TiO}_2$  catalysts than the  $\text{Sb}(2\%)/\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst which eventually supports the existence of high amount of ammonium bisulfate salt over  $\text{W}(10\%)/\text{V}_2\text{O}_5/\text{TiO}_2$  catalyst resulting in less resistance to sulfur ( $\text{SO}_2$ ) deactivation [21,23]. Consequently it can be concluded that large amount of tungsten promoter can be replaced by smaller amount of antimony for the low temperature and/or sulfur environment application.

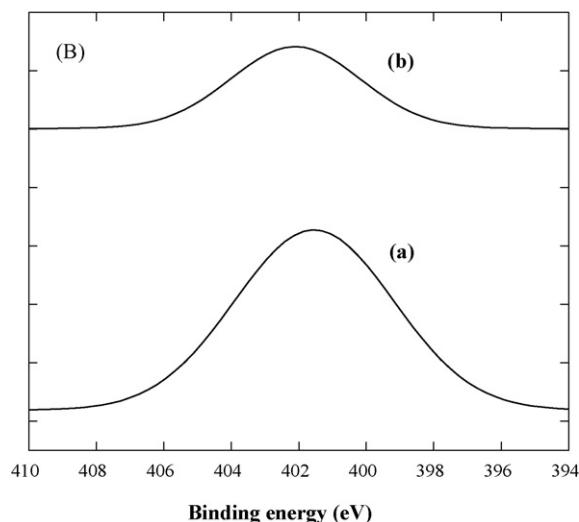
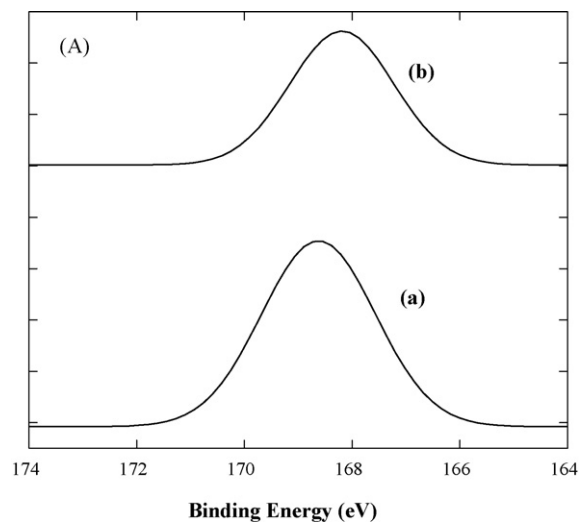


Fig. 10. XPS spectra of (A) S 2p and (B) N 1s of  $\text{SO}_2$  deactivation samples after 90 h (a)  $\text{W}/\text{V}_2\text{O}_5/\text{TiO}_2$  and (b)  $\text{Sb}/\text{V}_2\text{O}_5/\text{TiO}_2$ .

#### 4. Conclusions

Quantum chemical calculation study was carried out to select promoters which are capable of decreasing SO<sub>2</sub> deactivation on V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalysts. Among the selected promoters selenium, antimony, copper and sulfur showed for high NO<sub>x</sub> conversions at low temperatures. From the sulfur deactivation studies it is concluded that antimony promoted V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst is best for the low temperature SO<sub>2</sub> deactivation resistance. The high electrical conductivity change ( $\Delta G$ ) of Sb(2%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> than W(10%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst obtained during in situ electrical conductivity study and its correlation with high catalytic activity at low temperatures suggest that the Sb(2%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> is highly promising catalyst. The evidences and interpretations observed by the XPS, BET-SA and CHNS elemental analysis also confirmed the effective catalytic performance and resistance to SO<sub>2</sub> of Sb(2%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> than W(10%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> at low temperatures. Finally it is concluded that Sb(2%) promoted V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalyst can be efficiently used as sulfur resistance catalyst at low temperatures in substitution to commercial W(10%)V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub>.

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